

Millimeter-Wave Microstrip Patch Antenna Design for Future 5G Wireless Communication Systems

Himanshu Shukla¹, Prof. Sneha Jain²

^{1,2}Department of Electronic and Communication Engineering, RITS, Bhopal, MP, India

ABSTRACT

Various shapes of microstrip patch antenna had been designed in antenna field. This paper represents two patch element combined together and formed antenna array I have focus on the design and simulation of Microstrip patch antennas (which are widely used in cell phone today) with an emphasis on optimization of a 2.4 GHz to 3.42GHz circular probe fed patch antenna. I have found that different parameter like substrate dimension, μ , ϵ , patch radius, feed radius etc. affects the directivity, radiation efficiency, total efficiency and return loss curve of the patch antenna. I have analyzed the simulation result for far-field of different patch antenna and on comparing the parameter values of different patch antenna. I found an optimized patch antenna. I have designed and studied the simulated performance result of an optimized microstrip patch antenna using CST simulator. The rapid growth of wireless and satellite communication applications has provided an impetus for increased interest in the research and design of antennas with enhanced performance characteristics.

Keywords: *VSWR, Directivity, Antenna efficiency.*

I. INTRODUCTION

Antenna is a very interesting component in communication field. Antenna is responsible for converting sound waves into electromagnetic waves and vice-versa. Antenna also plays a very important role for transmission and reception process of signals from one place to another place. Due to the compactness the microstrip antennas are came into

existence. Various shapes [1,5] of microstrip patch are available for such as rectangular, square, circular, annular etc. The purpose of choosing triangular shape is the triangular waveforms can be easily calculated rather than other waveforms. Triangular microstrip patch antenna consists of a triangular shape radiating patch on one side of dielectric substrate which mounted on a ground plane. For getting the good performance of patch antenna we must be careful about the height, dielectric constant of material and operating frequency. Periodic structure has long been an active subject in the microwave community and has recently attracted considerable attention due to the incorporation of [2] electromagnetic band-gap (EBG) structures for enhancing antenna performance. In the proposed work, first of all an EBG structure has been designed on a dielectric substrate material. Then it has been employed to study microstrip patch antennas and arrays performance etched on another substrate layer. Thus, basic idea is to design the EBG substrate backed patch antenna, so that the band gap of EBG substrate and resonant frequency of patch antenna overlaps, therefore inhibiting the surface wave propagation. The feature of surface wave suppression helps to improve antenna's performance such as increasing the antenna gain and reducing back radiation in the case of finite antenna ground plane. In addition, the in-phase reflection feature leads to low profile antenna designs. A single patch has been investigated with the designed EBG [3] by varying number of EBG layers and their spacing with the patch. A novel design of an electromagnetic band-gap (EBG) structure using CST simulation software has been proposed for application in microstrip antennas. This EBG structure when

incorporated with microstrip patch antenna is found to increase its directivity remarkably. The designed EBG structures suppress propagation of surface waves at a particular band-gap frequency and have been found to decrease reflection loss significantly. The EBG structure has been designed for a band-gap 6.5 to 8.5 GHz [7]. This structure has been applied on a rectangular patch substrate with dielectric constant 6.6. The directivity using the designed structure has been found to be 8.626 dB at 7.5 GHz. The return loss curve has been improved by using EBG structure [4] of microstrip Patch antennas. This paper focuses on the hardware fabrication and software simulation of several antennas. In order to completely understand the above it is necessary to start off by understanding various terms associated with antennas and the various types of antennas. This is what is covered in this introductory.

II. ANTENNA PARAMETERS

An antenna is an electrical conductor or system of conductors Transmitter - Radiates electromagnetic energy into space Receiver - Collects electromagnetic energy from space The IEEE definition of an antenna as given by Stutzman and Thiele is, "That part of a transmitting or receiving system that is designed to radiate or receive electromagnetic waves". The major parameters associated with an antenna are defined in the following sections.

ANTENNA GAIN

Gain is a measure of the ability of the antenna to direct the input power into radiation in a particular direction and is measured at the peak radiation intensity. Consider the power density radiated by an isotropic antenna with input power P_0 at a distance R which is given by $S = P_0/4\pi R^2$. An isotropic [8] antenna radiates equally in all directions, and its radiated power density S is found by dividing the radiated power by the area of the sphere $4\pi R^2$. An isotropic radiator is considered to be 100% efficient. The gain of an actual antenna increases the power density in the direction of the peak radiation:

$$S = \frac{P_0 G}{4\pi R^2} = \frac{|E|^2}{\eta}$$

Or

$$|E| = \frac{1}{R} \sqrt{\frac{P_0 G \eta}{4\pi}}$$

Gain is achieved by directing the radiation away from other parts of the radiation sphere. In general, gain is defined as the gain-biased pattern of the antenna.

$$S(\theta, \phi) = \frac{P_0 G(\theta, \phi)}{4\pi R^2} \quad \text{Power Density}$$

$$U(\theta, \phi) = \frac{P_0 G(\theta, \phi)}{4\pi} \quad \text{Radiation Intensity}$$

ANTENNA EFFICIENCY

The surface integral of the radiation intensity over the radiation sphere divided by the input power P_0 is a measure of the relative power radiated by the antenna, or the antenna efficiency.

$$\frac{P_r}{P_0} = \int_0^{2\pi} \int_0^\pi \frac{G(\theta, \phi)}{4\pi} \sin\theta \, d\theta \, d\phi = \eta_e$$

Where P_r is the radiated power. Material losses in the antenna or reflected power due to poor impedance match reduce the radiated power.

EFFECTIVE AREA

Antennas capture power from passing waves and deliver some of it to the terminals. Given the power density of the incident wave and the effective area of the antenna, the power delivered to the terminals is the product.

$$P_d = S A_{eff}$$

For an aperture antenna such as a horn, parabolic reflector, or flat-plate array, effective area is physical area multiplied by aperture efficiency. In general, losses due to material, distribution, and mismatch reduce the ratio of the effective area to the physical area. Typical estimated aperture efficiency for a parabolic reflector is 55%. Even antennas with infinitesimal physical areas, such as dipoles, have effective areas because they remove power from passing waves.

DIRECTIVITY

Directivity is a measure of the concentration of radiation in the direction of the maximum.

$$\text{Directivity} = \frac{\text{maximum radiation intensity}}{\text{average radiation intensity}} = \frac{U_{\max}}{U_0}$$

Directivity and gain differ only by the efficiency, but directivity is easily estimated from patterns. Gain—directivity times efficiency—must be measured. The average radiation intensity can be found from a surface integral over [9] the radiation sphere of the radiation intensity divided by 4π , the area of the sphere in steradians:

average radiation intensity

$$= \frac{1}{4\pi} \int_0^{2\pi} \int_0^\pi U(\theta, \phi) \sin\theta \, d\theta \, d\phi = U_0$$

This is the radiated power divided by the area of a unit sphere. The radiation intensity $U(\theta, \phi)$ separates into a sum of co- and cross-polarization components:

$$U_0 = \frac{1}{4\pi} \int_0^{2\pi} \int_0^\pi [U_c(\theta, \phi) + U_x(\theta, \phi)] \sin\theta \, d\theta \, d\phi$$

Both co- and cross-polarization directivities can be defined:

$$\text{Directivity}_c = \frac{U_{c,\max}}{U_0}$$

Directivity can also be defined for an arbitrary direction $D(\theta, \phi)$ as radiation intensity divided by the average radiation intensity, but when the coordinate angles are not specified, we calculate directivity at U_{\max} .

PATH LOSS

We combine the gain of the transmitting antenna with the effective area of the receiving antenna to determine delivered power and path loss. The power density at the receiving antenna is given by equation and the received power is given by equation by combining the two, we obtain the path loss as given below

$$\frac{P_d}{P_t} = \frac{A_2 G_1(\theta, \phi)}{4\pi R^2}$$

Antenna 1 transmits, and antenna 2 receives. If the materials in the antennas are linear and isotropic, the transmitting and receiving patterns are identical. When we consider antenna 2 as the transmitting antenna and antenna 1 as the receiving antenna, the path loss is

$$\frac{P_d}{P_t} = \frac{A_1 G_2(\theta, \phi)}{4\pi R^2}$$

We make quick evaluations of path loss for various units of distance R and for frequency

f in megahertz using the formula

$$\text{path loss}(dB) = K_v + 20 \log(f R) - G_1(dB) - G_2(dB)$$

where K_v depends on the length units as shown in table 1.

Table 1

Unit	K_v
km	32.45
nm	37.80
miles	36.58
m	-27.55
ft	-37.87

INPUT IMPEDENCE

The input impedance of an antenna is defined as “the impedance presented by an antenna at its terminals or the ratio of the voltage to the current at the pair of terminals or the ratio of the appropriate components of the electric to magnetic fields at a point”. Hence the impedance of the antenna can be written as given below.

$$Z_{in} = R_{in} + jX_{in}$$

where Z_{in} is the antenna impedance at the terminals
 R_{in} is the antenna resistance at the terminals
 X_{in} is the antenna reactance at the terminals

The imaginary part, X_{in} of the input impedance represents the power stored in the near field of the antenna. The resistive part, R_{in} of the input impedance consists of two components, the radiation resistance R_r and the loss resistance R_L [10]. The power associated with the radiation resistance is the power actually radiated by the antenna, while the power dissipated in the loss resistance is lost as heat in the antenna itself due to dielectric or conducting losses.

III. ANTENNA FACTOR

The engineering community uses an antenna connected to a receiver such as a spectrum analyzer, a network analyzer, or an RF voltmeter to measure field strength E . Most of the time these devices have a load resistor Z_L that matches the antenna impedance.

The incident field strength E_i equals antenna factor AF times the received voltage V_{rec} .

We relate this to the antenna effective height:

$$AF = \frac{E_i}{V_{rec}}$$

AF has units meter^{-1} but is often given as $\text{dB}(\text{m}^{-1})$. Sometimes, antenna factor is referred to [12] the open-circuit voltage and it would be one-half the value given by equation. We assume that the antenna is aligned with the electric field; in other words, the antenna polarization is the electric field component measured:

$$AF = \sqrt{\frac{\eta}{Z_L A_{eff}}} = \frac{1}{\lambda} \sqrt{\frac{4\pi}{Z_L G}}$$

This measurement may be corrupted by a poor impedance match to the receiver and any cable loss between the antenna and receiver that reduces the voltage and reduces the calculated field strength.

RETURN LOSS

It is a parameter which indicates the amount of power that is “lost” to the load and does not return as a reflection. Hence the RL is a parameter to indicate how well the matching between the transmitter and antenna has taken place. Simply put it is the S_{11} of an antenna. A graph of s_{11} of an antenna vs frequency is called its return loss curve. For optimum working such a graph

must show a dip at the operating frequency and have a minimum dB value at this frequency. This parameter was found to be of crucial importance to our paper as we sought to adjust the antenna dimensions for a fixed operating frequency (say 2.4 GHz). A simple RL curve is shown in figure 1.

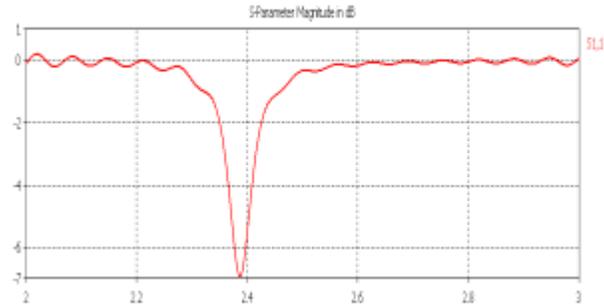


Figure 1: RL curve of an antenna

RADIATION PATTERN

The radiation pattern of an antenna is a plot of the far-field radiation properties of an antenna as a function of the spatial co-ordinates which are specified by the elevation angle (θ) and the azimuth angle (ϕ). More specifically [11] it is a plot of the power radiated from an antenna per unit solid angle which is nothing but the radiation intensity. It can be plotted as a 3D graph or as a 2D polar or Cartesian slice of this 3D graph. It is an extremely parameter as it shows the antenna's directivity as well as gain at various points in space. It serves as the signature of an antenna and one look at it is often enough to realize the antenna that produced it.

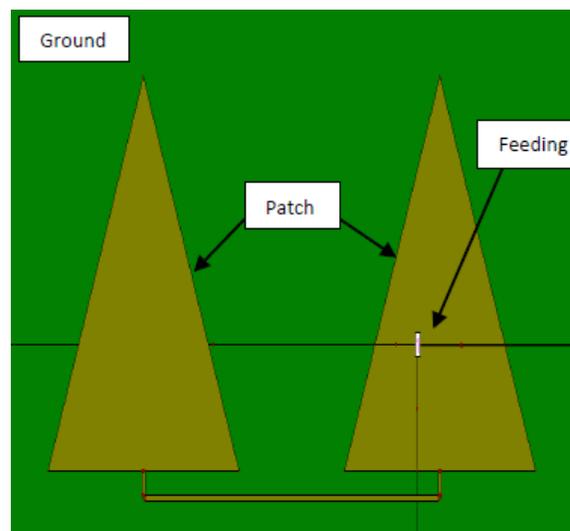


Fig.2: Patch element antenna array

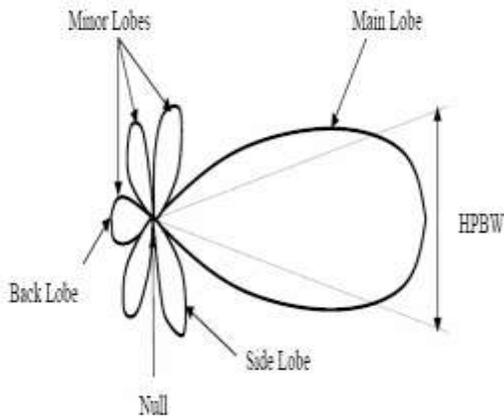


Fig.3: radiation pattern of HPBW from

Beam width of an antenna is easily determined from its 2D radiation pattern and is also a very important parameter. Beam width is the angular separation of the half-power points of the radiated pattern. The way in which beam width Microstrip antennas are planar resonant cavities that leak from their edges and radiate. Printed circuit techniques can be used to etch the antennas on soft substrates to produce low-cost and repeatable antennas in a low profile. The antennas fabricated on compliant substrates withstand tremendous [15] shock and vibration environments. Manufacturers for mobile communication base stations often fabricate these antennas directly in sheet metal and mount them on dielectric posts or foam in a variety of ways to eliminate the cost of substrates and etching. This also eliminates the problem of radiation from surface waves excited in a thick dielectric substrate used to increase bandwidth.

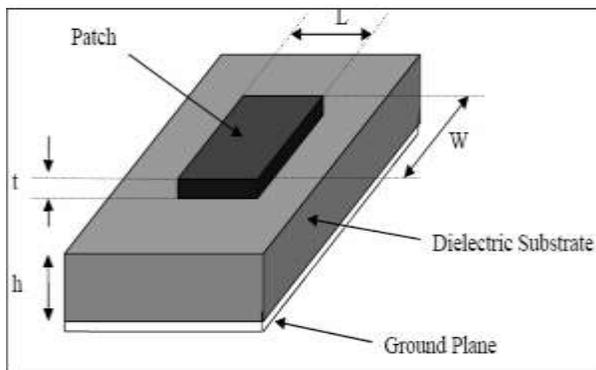


Fig.4: Microstrip Patch Antenna

I have designed large number of patch antenna by varying different parameters like μ_r , ϵ_r , substrate dimension ,patch radius and feed radius. I have studied the [16] simulation result for far-field for different patch antenna and on comparing the parameters values for different patch antenna we found an optimized patch antenna. I have found directivity = 7.166 dB, radiation efficiency = -0.157 dB and total efficiency = -0.527 dB.

IV. RESULTS

The proposed EBG-based antenna design consists of 2.4 GHz to 3.42GHz drilled holes on a dielectric substrate. Parameters that described an EBG structure are radius and periodicity of the structures (drilled holes/cylindrical rods). Fig. shows the proposed antenna design with EBG and without EBG.

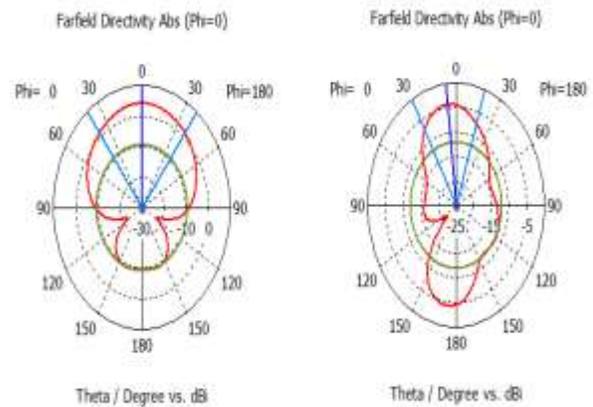


Fig.5: Polar plot of directivity for phi and patch antenna

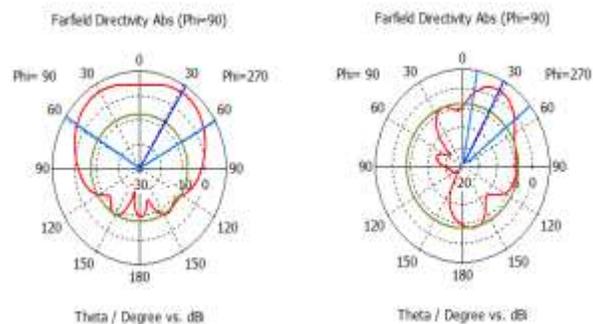


Fig.6: Polar plot of Directivity 90 for phi = 90 for EBG patch antenna

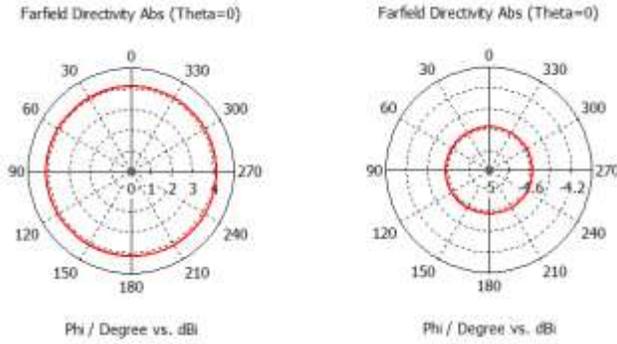


Fig.7: plot of directivity for theta = 0 for simple patch = 0 for EBG antenna

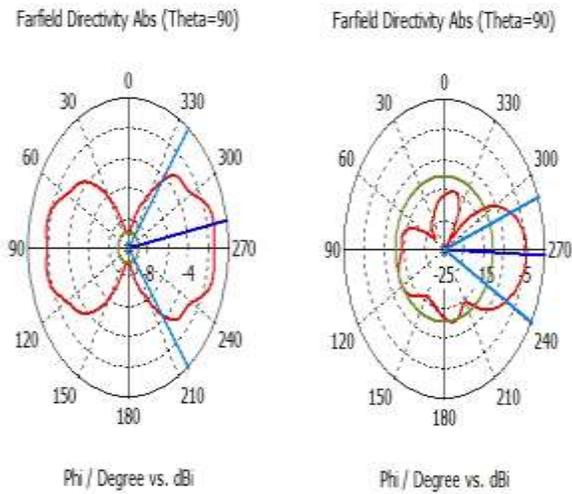


Fig.8: Plot theta = 90 for antenna, directivity for theta = 90 EBG based antenna

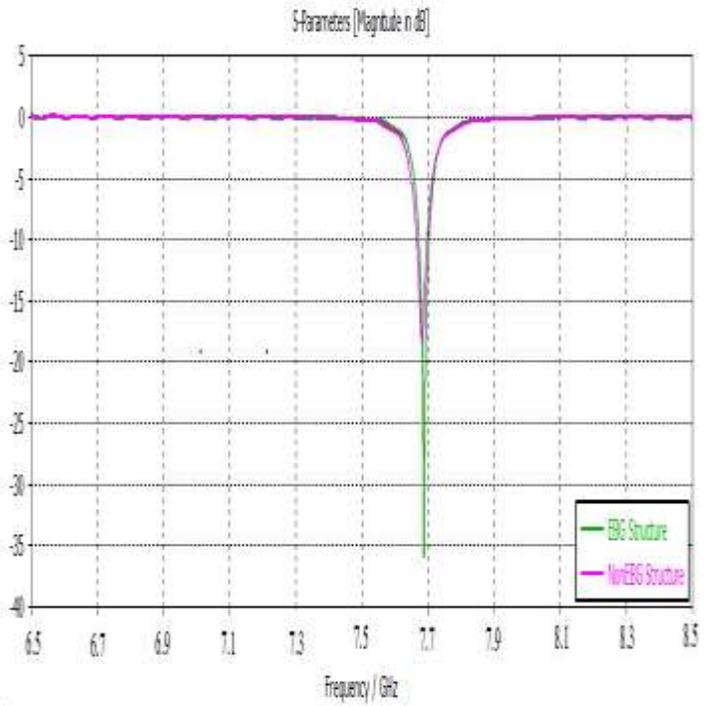


Fig.9: Reflection Loss curve Patch antenna and EBG without EBG structure antenna

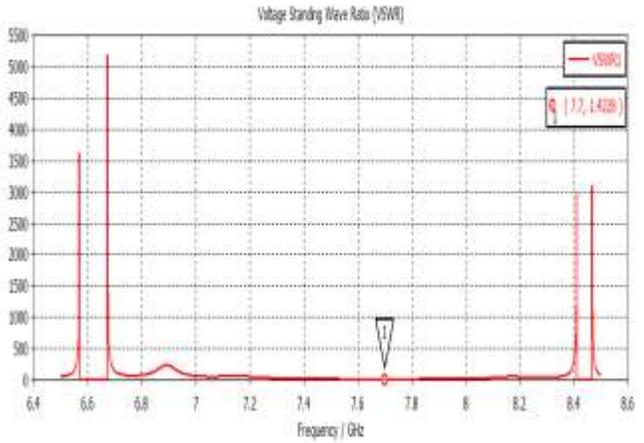


Fig.10. VSWR Curve of Non EBG Structure of Patch Antenna

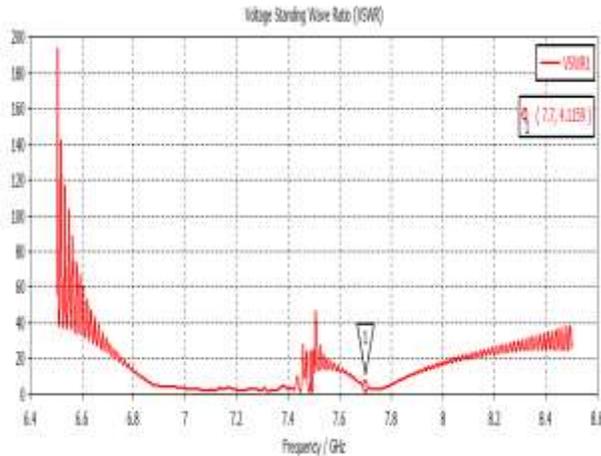


Fig. 11: VSWR Curve of EBG Structure of Patch Antenna

V. CONCLUSION

A novel electromagnetic band-gap structure has been also designed and analyzed in this thesis using finite-difference time-domain solver and its incorporation in a microstrip patch antenna for improvement of gain has been investigated. The designed EBG structure is a periodic rectangular lattice of drilled holes (radius = 4.32 mm with periodicity 10 mm) giving a band-gap of 6.5-8.5 GHz. These structures have been implemented on a rectangular patch of size 7 mm × 10 mm on a substrate with dielectric constant 6.7. A remarkable improvement in gain was observed when the patch substrate is replaced with the EBG-based substrate due to suppression of surface waves by the air-dielectric inside EBG structure. Thus, this EBG-based microstrip antenna design can be considered suitable for wireless communication requiring moderate bandwidth and high gain. It is known that the gain of the antenna can be increased by reducing any loss of the antenna. Selection of a good quality (low-loss) substrate will reduce the dielectric and conductor losses. However, surface waves travel inside the substrate and reduce the gain. To reduce this surface wave loss, wave propagation has to be stopped inside or reflected outside the substrate to enhance the gain in forward direction. The waves are arrested or retarded by obstructing their path with a high propagation impedance air ($\epsilon_r = 1$). The impedance offered by a dielectric is given as $Z_0 = \eta / \sqrt{\epsilon_r}$. This implies that the impedance offered is maximum for smallest value

of ϵ_r (the smallest value of ϵ_r being 1 for air). In the proposed antenna, the surface waves are reduced by drilling holes in periodic fashion in the dielectric substrate. The remarkable improvement in Directivity can be attributed to the periodic effect of embedding EBG patches in the substrate.

VI. FUTURE WORK

In this paper, we examined a circular probe fed patch antenna and the use of EBG structure on the feedline to help improve the directivity. The future work can involve changing the antenna type (including antenna shape and the dielectric of the substrate) and carry out further research into the EBG structures. Besides, we can also use different shapes of microstrip patches such as square shape and circular shape patch to carry out the research. While examining, similar EBG patterns proposed in the paper can be etched on the feedline of the proposed new antennas. Hence, one can formulate the results for every kind of patch shape for a patch antenna.

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